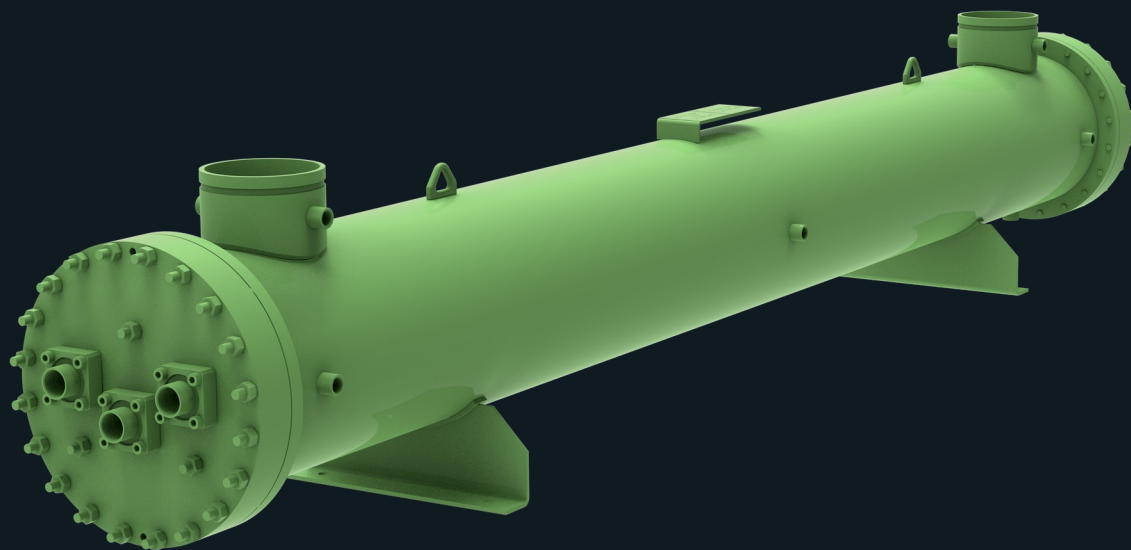




DRY-EXPANSION / STRAIGHT TUBE EVAPORATORS

PURE COOLER



DP-259-1 // ASME



HEAT
EXCHANGERS

BITZER US Pressure Vessels

In addition to our shell and tube heat exchangers, receivers, and oil separators, BITZER US also delivers high quality pressure vessels that meet the demand for industrial Ammonia and CO₂ applications. These vessels are commonly used in cold storage facilities, ice makers, supermarkets, and other industrial processing systems.

BITZER US utilizes multiple welding stations that provide fast, consistent, and reliable welds which results in high quality vessels with short lead times. All vessels are manufactured in the USA and in accordance with the most recent edition of Section VIII, Division 1 of the ASME code or other certifications as required.

Design Capabilities

- Max Diameter: 96"
- Max Length: 290"
- Max Pressure: 3000 PSI
- Min Temperature: -55°F

Testing

- Ultrasonic
- Penetrant
- Decay Test

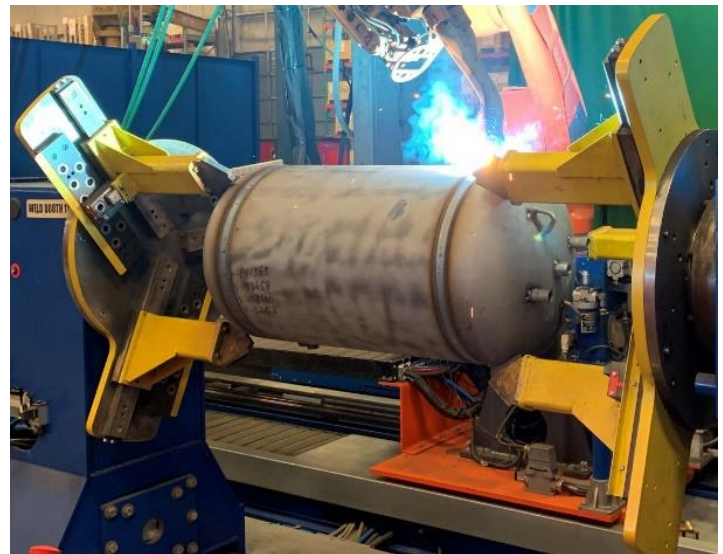
Certifications

- ASME
- PED
- CRN
- DOSH

Manufacturing

- Robotic Welding
- Water Jet
- Pipe Cutter
- Plasma Table
- CNC Machine Shop

Vessel Factory (USA)





NEW Shell-and-Tube Dry Expansion Evaporators: PURE COOLER

In keeping with the BITZER strategy of offering the most advanced design and technology, the PURE COOLER Evaporators utilize a high efficiency, counter current, single-pass design for maximum efficiency, reliability, and performance.

The PURE COOLER Evaporators are specially designed and optimized for R134a (and similar refrigerants) to meet the latest system and building efficiency requirements by providing performance that rivals flooded evaporators.

NEW Improvements with PURE COOLER

- Innovative and patented distribution improves refrigerant heat transfer and optimized for R134a
- Optimized plastic baffles decrease leakage and improve brine side heat transfer
- Special inner grooved pattern of tubes maximizes heat transfer coefficient and limit negative effects of pressure drop specifically with R134a

Performance Advantages

- Optimized for refrigerant R134a, and similar lower GWP refrigerants like R450A, R513A, R1234yf, R1234ze
- Maximum efficiency utilizing latest shell-and-tube technology to enhance heat transfer improvement
- Robotic welding technology used for optimum quality and product appearance
- Worldwide BITZER engineering and pressure vessel testing, design, and experience
- All products are made in the USA

“Future Proof” Technology

- R134a is already widely used in a variety of applications as a common A1 refrigerant with a Global Warming Potential (GWP) of 1430
- Near drop-in alternative refrigerants R450A and R513A are growing in popularity as A1 refrigerants with half the GWP of R134a
- HFO refrigerants R1234yf and R1234ze(E) which are A2L have negligible GWP and could be future substitutes as systems gravitate towards mildly flammable designs

ASME Design Safety

BITZER ASME evaporators are manufactured in accordance with the latest edition of ASME Section VIII, Division 1, and are designed for use in air-conditioning and refrigeration applications. CRN is available on majority of models. Consult factory for PED (CE) availability.



Design Specifications

- Refrigerant side:
 - All Models: 240 psi @ -4° to 140°F
- Shell / Water side:
 - All Models: 145 psi @ -4° to 140°F

Explanation of Model Number

P C A D 3 2 6 - 3 H - T F K

Product Series

PCA = Pure Cooler Shell and Tube Evaporator (ASME Rated)

P C A D 3 2 6 - 3 H - T F K

Number of Circuits

S = One
D = Two
T = Three
Q = Four

P C A D 3 2 6 - 3 H - T F K

Shell Diameter Designation

16 = 6 NPS
19 = 8 NPS
21 = 8 NPS
27 = 10 NPS
32 = 12 NPS
40 = 16 NPS
50 = 20 NPS

P C A D 3 2 6 - 3 H - T F K

Tube Number Designation (6,7,8,9)

P C A D 3 2 6 - 3 H - T F K

Tube Length Designation (1,2,3)

P C A D 3 2 6 - 3 H - T F K

Flow Type / Baffle Spacing (Optional)

H = Low Flow

P C A D 3 2 6 - 3 H - T F K

Water Connection Location

T = Top (Standard)
L = Left
R = Right

P C A D 3 2 6 - 3 H - T F K

Water Connection Type

F = Flange Connections (Standard)
J = Flexible Joint Connections

P C A D 3 2 6 - 3 H - T F K

Additional Options

K = ¾ in. Thick insulation
M = 1 ½ in. Thick Insulation

Selecting the Right Heat Exchanger

Selecting a heat exchanger by a table or chart can be challenging because many parameters and requirements are involved. These factors affect one another and lead to an iterative process to reach a suitable selection. Furthermore, one selection may be valid for a certain set of conditions; however, A/C and refrigeration systems operate a wide range of seasonal loads and conditions that must also be considered by the system designer.

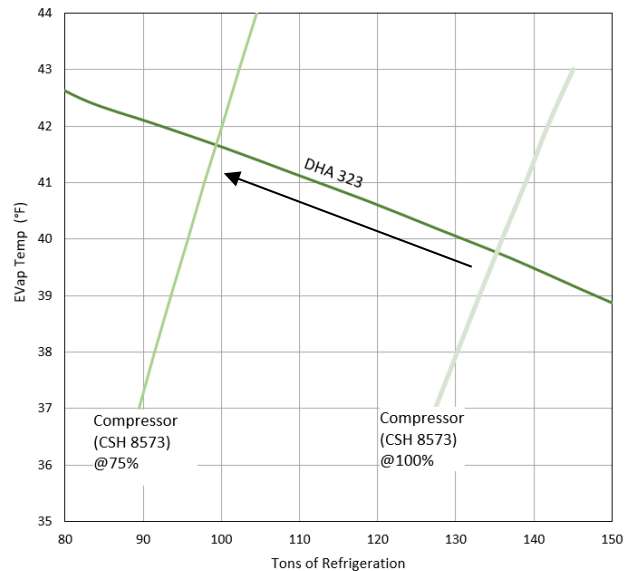
Therefore, it is strongly recommended to use the **smarTube** sizing software or consult BITZER USA for assistance. The following pages are provided as a guideline to help steer the decision process and better understand heat exchangers and the inputs that **smarTube** requires. Download **smarTube** from www.bitzerus.com.

Heat Exchanger Operating Point

For a set of conditions, the evaporator will operate at a saturated evaporating temp (**Evap Temp**) that is balanced with the operation of the compressor.

If the cooling load is reduced and the compressor reduces its Capacity, the Flow Rate of the process fluid should also be reduced which results in a new operating point at the lower Capacity, but higher Evap Temp.

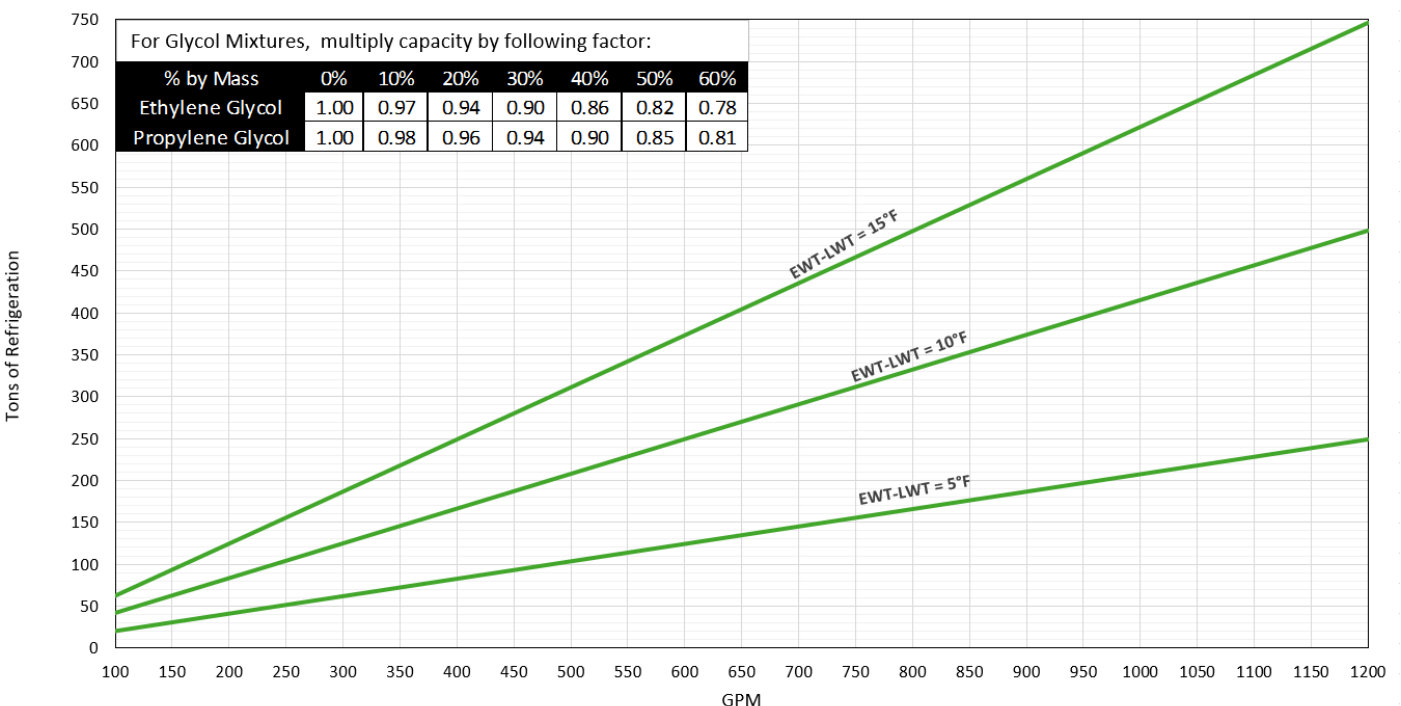
The difference in Leaving Water Temp and Evap Temp is called the **Approach**. A lower Approach is desirable because it increases the Evap Temp; thus, the compressor will operate at a higher suction pressure with increased capacity and efficiency. For glide refrigerants, the dew point of the Evap Temp is implied when referenced in this document.



Capacity of Heat Exchangers (Fluid "Water" Side)

The **Capacity** of a shell and tube evaporator is calculated using the Flow Rate, the Range, and the specific heat of the process fluid. The **Flow Rate** is a measurement of the volumetric rate, often in gallons per minute (GPM). The **Range** refers to the temperature change of the process fluid and is calculated by subtracting the Leaving Water Temp (LWT) from the Entering Water Temp (EWT). For any given fluid, 3 of the following 4 requirements must be specified: Capacity, Flow Rate, EWT, and LWT. The result of the remaining parameter can then be calculated.

The following chart shows capacities for water at varying Flow Rates and Ranges with multipliers for glycol mixtures.





The Pure Cooler series of evaporators cover a broad range of capacities but have limitations due to maximum and minimum flowrates. A lower flow may reduce heat transfer while a higher flow may create undesirable pressure drop for pumps to overcome. In addition, an optimal velocity range is necessary to prevent fouling at the tube surface.

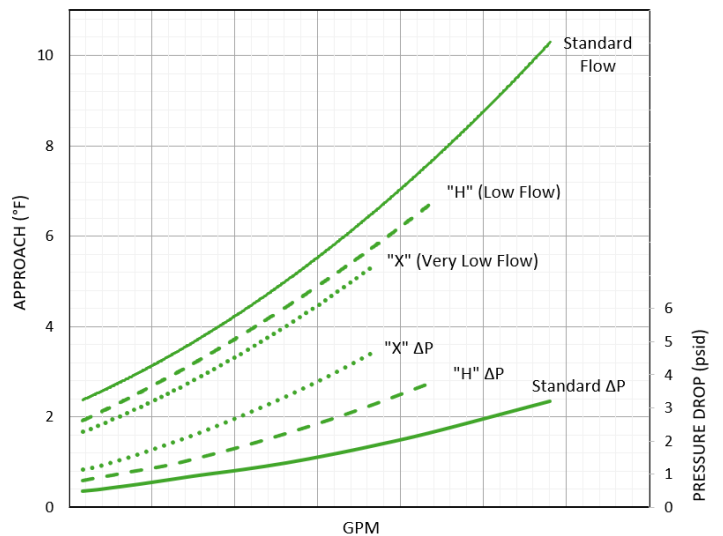
Model	Shell Dia. (NPS)	Available Circuits				Capacity at Max Flow $\Delta 10^{\circ}\text{F}$ (TR)	Capacity At Min Flow $\Delta 10^{\circ}\text{F}$ (TR)	Maximum Flow Rate (GPM)	Minimum Flow Rate (GPM)	Water Pressure Drop at Max Flow (psid)	
		1	2	3	4						
PCA_-226-1	8	√	√	√		58.0	29.0	139.8	70.0	3.6	
PCA_-227-1		√	√			73.3	29.9	176.6	72.0	5.4	
PCA_-227-2		√	√			93.6	27.4	225.7	66.0	10.0	
PCA_-276-2	10	√	√	√		118.0	35.3	284.5	85.0	9.2	
PCA_-277-2		√	√	√		134.3	36.5	323.8	88.0	11.2	
PCA_-326-2	12	√	√	√		164.8	49.8	397.4	120.0	9.0	
PCA_-328-2		√	√			209.6	69.7	505.3	168.0	7.7	
PCA_-416-2	16	√	√	√	√	236.0	91.3	569.1	220.0	5.5	
PCA_-416-3				√	√	√	263.1	103.7	634.3	250.0	5.3
PCA_-419-2		√	√	√	√	307.8	87.1	742.2	210.0	9.9	
PCA_-419-3			√	√	√	307.8	97.5	742.2	235.0	8.1	
PCA_-516-2	20		√	√	√	386.6	149.3	932.1	360.0	5.5	
PCA_-516-3			√	√	√	386.7	160.9	932.2	388.0	4.7	
PCA_-519-2			√	√	√	480.1	153.5	1157.5	370.0	8.0	
PCA_-519-3			√	√	√	480.1	161.8	1157.6	390.0	7.0	
PCA_-618-3	24		√	√	√	602.8	170.1	1453.3	410.0	9.6	
PCA_-6110-3			√	√	√	602.8	181.8	1453.3	438.2	9.5	

- Data valid for 1 and 2 circuits only
- Max capacity may not be possible depending on refrigerant selection and limitation of refrigeration velocity
- Data calculated with 100% Water (Glycol mixtures will have higher pressure drops and lower capacity)
- $\Delta 10^{\circ}\text{F}$ is the Range = Entering Water Temp – Leaving Water Temp
- Flow Rates are established using a combination of max / min velocity and pressure drops (min p drop = ~1 psid)
- Lower Flow Rates possible using "H" models
- 1 TR = 12,000 BTU/h

Low Flow Models – "H"

As the Flow Rate decreases for a given model, the Approach of the heat exchanger improves although water velocity may be too low for extended operation. In a low flow situation (usually $>\Delta 10^{\circ}\text{F}$ Range), a higher water velocity to reduce fouling is possible by adding additional baffles to the heat exchanger. These baffles increase pressure drop but also further improve heat transfer and efficiency.

The addition of glycol to water increases viscosity and, thus, also increases the pressure drop.



Performance Data: Capacity and Approach

The following graphs charts the performance of the PCA catalog using one refrigerant (note chart conditions). A larger heat exchanger will result in a smaller Approach but may have limitations in lower flowrates. Depending on the system, it is recommended to select a heat exchanger based on design conditions near the upper end (60 to 90%) of the curve so that in long periods of turndown (reduced capacity), the heat exchanger can operate with sufficient fluid flow.

In addition to capacity, Approach, Flow Rate and refrigerant, many other factors will affect the rating of the heat exchange such as Range, Fouling Factor, Liquid Temp, and Superheat. Always be sure the Approach does not allow the saturation evaporating temperature to fall below the freezing point of the process fluid. Use **smarTube** sizing software or consult BITZER USA for final design.

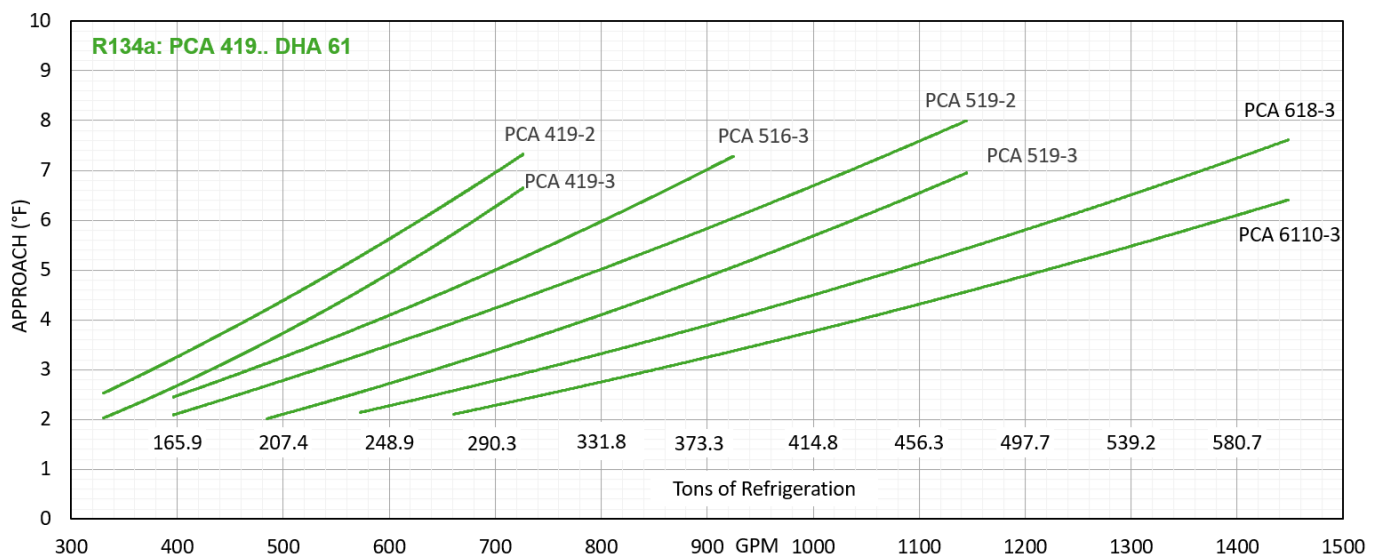
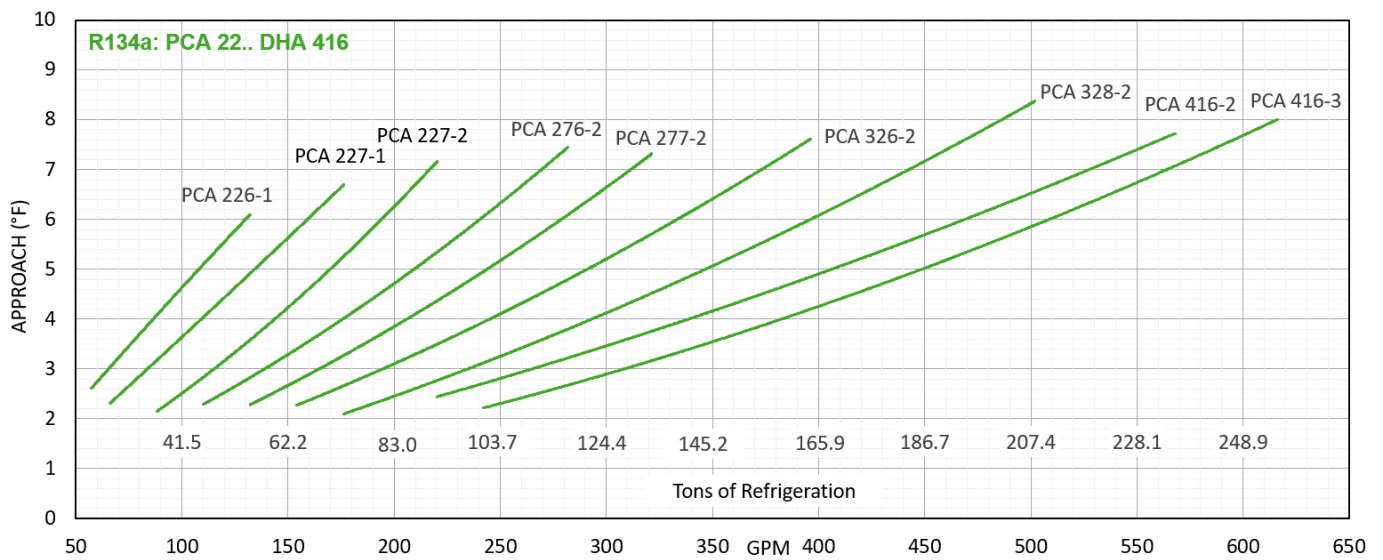


Chart Conditions: Water | EWT 54°F | LWT 44°F | Fouling .0001 ft²h°F/BTU | Liquid Temp 100°F | Superheat 7°ΔF



Performance Data – Refrigerants

The PCA series is capable of working with other refrigerants. However, showing performance curves for all refrigerants is not practical.

In the displayed graph, a comparison of refrigerants (using the same heat exchanger and input factors) provides an idea of the difference between the refrigerants and the approximate impact on the Approach.

The calculation for Approach uses the dew point of the Evap Temp. For this reason, glide refrigerants have an Approach that is better in contrast with using the mean evaporating temperature.

Performance Data – Efficiency Factors

As mentioned previously, certain factors must be considered to appropriately select your heat exchanger. Some factors will change over seasons or time, such as liquid temp or fouling, while others are set at commissioning, such as superheat.

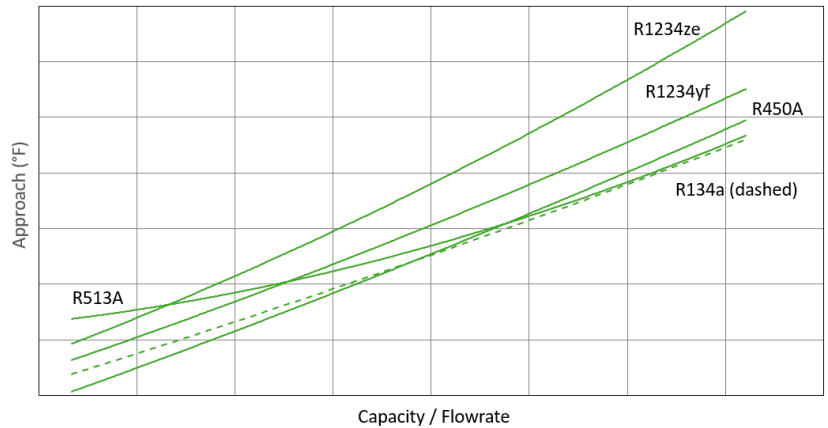
Each of these factors affect the efficiency of the heat exchanger which changes the Evap Temp and Approach. These three charts are provided to illustrate this change in Approach based on a factor, assuming other conditions are held constant.

Fouling is the accumulation of dirt and deposits onto the heat exchange surface. Although this can occur on both inside and outside of tubes, usually the water side is the primary consideration. Fouling reduces heat transfer and therefore requires a lower Evap Temp (higher Approach) to maintain the same capacity.

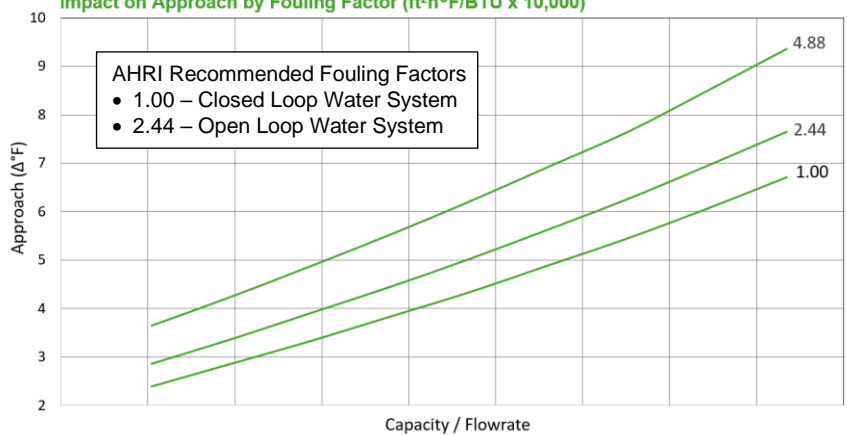
Superheat shrinks the area of the heat exchanger used for latent heat absorption. The decrease in heat exchange area requires a lower Evap Temp (higher Approach) to maintain the same capacity.

Finally, an increase in **Liquid Temp** increases the quality (vapor content) of the refrigerant after the expansion valve resulting in reduction of capacity. Hence, the Evap Temp is lowered (or Approach increased) to maintain the same capacity.

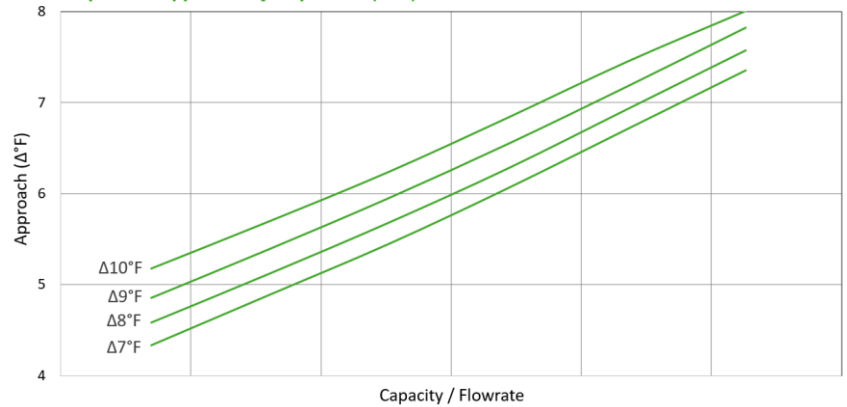
Impact on Approach by Refrigerant Type



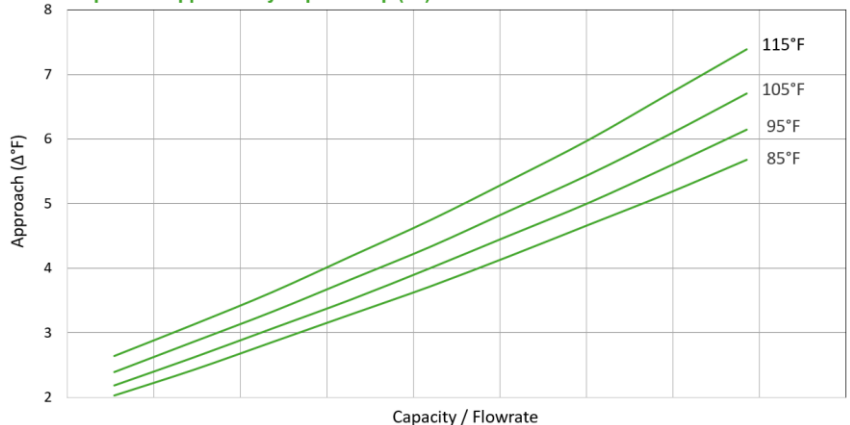
Impact on Approach by Fouling Factor (ft²h⁰F/BTU x 10,000)



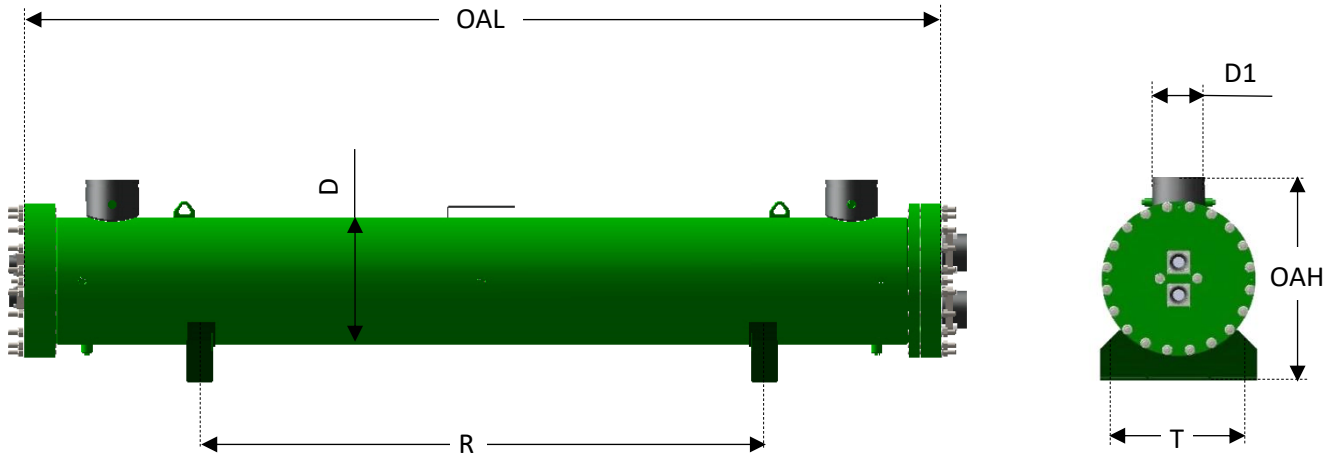
Impact on Approach by Superheat (Δ°F)



Impact on Approach by Liquid Temp (°F)



Dimensions



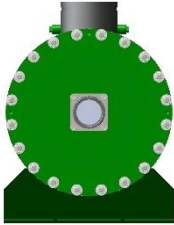
Model	Dimensions			Feet		Connection								Volumes-Weights			
	OAL	D	OAH	R	T	"S" 1 Circuit		"D" 2 Circuit		"T" 3 Circuit		"Q" 4 Circuit		Water Conn. D1	Wt.	Vol. Tube side	Vol. Shell side
						Ref. Inlet	Ref. Outlet	Ref. Inlet	Ref. Inlet	Ref. Outlet	Ref. Outlet	Ref. Outlet	Ref. Outlet				
	in	in	in	in	in	in	in	in	in	in	in	in	in	NPS	Lbs.	ft ³	ft ³
PCA_-226-1	92 1/2	8-5/8	15 3/4	63	10 1/4	1 5/8	3 1/8	1 1/8	2 5/8	1 1/8	2 5/8	-	-	3	366	0.7	2.0
PCA_-227-1	92 1/4	8-5/8	15 3/4	63	10 1/4	1 5/8	3 1/8	1 3/8	2 5/8	-	-	-	-	4	352	0.8	1.9
PCA_-227-2	113 7/8	8-5/8	15 3/4	70 7/8	10 1/4	1 5/8	3 1/8	1 3/8	2 5/8	-	-	-	-	4	505	1.0	2.3
PCA_-276-2	114 5/8	10-3/4	18 5/8	70 7/8	11 3/4	2 1/8	4 1/4	1 3/8	3 1/8	1 3/8	2 5/8	-	-	5	615	1.3	3.8
PCA_-277-2	114 5/8	10-3/4	18 5/8	70 7/8	11 3/4	2 1/8	4 1/4	1 3/8	3 1/8	1 3/8	2 5/8	-	-	5	630	1.4	3.6
PCA_-326-2	115 5/8	12-3/4	20 5/8	70 7/8	11 3/4	2 5/8	4 1/4	1 5/8	3 1/2	1 3/8	3 1/8	-	-	6	815	1.8	5.5
PCA_-328-2	115 5/8	12-3/4	20 5/8	70 7/8	11 3/4	2 5/8	5 1/4	1 5/8	3 1/2	1 3/8	3 1/8	-	-	6	830	2.3	5.0
PCA_-416-2	115 3/4	16	25 1/2	70 7/8	15 3/4	3 1/8	4 1/4	2 1/8	4 1/4	1 5/8	3 1/8	1 3/8	2 5/8	6	1300	2.6	9.0
PCA_-416-3	139 1/2	16	25 1/2	86 5/8	15 3/4	3 1/8	4 1/4	2 1/8	4 1/4	2 1/8	3 1/2	1 5/8	3 1/8	8	1425	3.1	10.8

Notes:

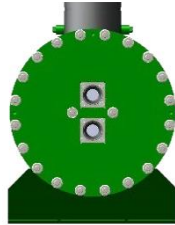
- All vessels are equipped with multiple couplings 1/2"NPT on shell as drain
- Two 3/4"NPT coupling on the opposite side of the brine connection as
- Dimensions are provided as a general and relative sizing guideline
- Individualized submittal drawings override dimensions and specifications shown here



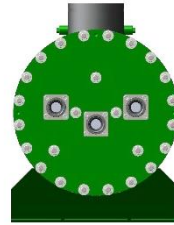
Dimensions



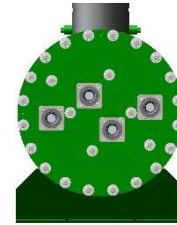
“S” 1 Circuit



“D” 2 Circuit



“T” 3 Circuit



“Q” 4 Circuit

Model	Dimensions			Feet		Connection								Volumes-Weights			
	OAL	D	OAH	R	T	“S” 1 Circuit		“D” 2 Circuit		“T” 3 Circuit		“Q” 4 Circuit		Water Conn. D1	Wt.	Vol. Tube side	Vol. Shell side
						Ref. Inlet	Ref. Outlet	Ref. Inlet	Ref. Inlet	Ref. Outlet	Ref. Outlet	Ref. Outlet	Ref. Outlet				
	in	in	in	in	in	in	in	in	in	in	in	in	in	NPS	Lbs.	ft ³	ft ³
PCA_-419-2	115 3/4	16	25 1/2	70 7/8	15 3/4	3 1/8	4 1/4	2 1/8	4 1/4	1 5/8	3 1/8	1 3/8	2 5/8	8	1340	3.4	8.0
PCA_-419-3	139 1/2	16	25 1/2	86 5/8	15 3/4	3 1/8	4 1/4	2 1/8	4 1/4	2 1/8	3 1/2	1 5/8	3 1/8	8	1470	4.1	9.7
PCA_-516-2	116 1/4	20	29 1/2	70 7/8	13 3/4	-	-	2 5/8	5 1/4	2 1/8	4 1/4	2 1/8	3 1/2	8	2080	4.7	10.6
PCA_-516-3	139 1/2	20	29 1/2	86 5/8	13 3/4	-	-	2 5/8	5 1/4	2 5/8	4 1/4	2 1/8	4 1/4	10	1825	5.5	16.5
PCA_-519-2	116 1/4	20	29 1/2	70 7/8	13 3/4	-	-	2 5/8	5 1/4	2 1/8	4 1/4	2 1/8	3 1/2	10	1690	5.7	12.4
PCA_-519-3	139 1/2	20	29 1/2	86 5/8	13 3/4	-	-	2 5/8	5 1/4	2 5/8	4 1/4	2 1/8	4 1/4	10	1800	6.8	15.1
PCA_-618-3	140 1/8	24	34 5/8	86 5/8	17 3/8	-	-	3 1/2	4 1/4	2 1/8	4 1/4	2 5/8	5 1/4	12	3690	8.2	22.6
PCA_-6110-3	140 1/8	24	34 5/8	86 5/8	17 3/8	-	-	3 1/2	4 1/4	2 1/8	4 1/4	2 5/8	5 1/4	12	3760	9.3	21.5



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